

## Design And Simulation Noise Characteristics of AlGa<sub>0.3</sub>N/GaN/AlGa<sub>0.06</sub>N/GaN HEMT on SiC Substrate For Low Noise Applications

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**Abstract:** In this paper, AlGa<sub>0.3</sub>N/GaN/AlGa<sub>0.06</sub>N/GaN high electron mobility transistor (HEMT) with 0.25 μm gate-length have been designed on an SiC-4H substrate. DC and Noise characteristics of AlGa<sub>0.3</sub>N/GaN/AlGa<sub>0.06</sub>N/GaN HEMT with 0.25 μm gate-length at microwave frequencies have been explored. The simulation has been performed by using the Silvaco software. The extrinsic transconductance of the device was 350 mS/mm. Also, device exhibited current drive capability as high as 1750 mA/mm. The device has demonstrated high unity current gain cut-off frequency (f<sub>t</sub>) of 200 GHz. The microwave noise characteristics of the device were determined from 0 to 20 GHz at different drain biases and drain currents. At a gate bias of -3 V and drain bias of 10 V, device exhibited a minimum noise figure (NF<sub>min</sub>) of 0.35 dB and maximum associated gain (G<sub>ma</sub>) of 24.35 dB at 10 GHz. The noise resistance of device is 7.2 ohm at 10 GHz, which is very suitable for low noise applications in X-band frequency range. These results indicates the capability of AlGa<sub>0.3</sub>N/GaN HEMT for low noise and high power amplifiers.

**Keywords:** AlGa<sub>0.3</sub>N, GaN, HEMT, microwave noise, minimum noise figure

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### I. Introduction

For microwave high-power and low noise applications AlGa<sub>0.3</sub>N/GaN HEMT attracted consideration because of their excellent microwave characteristics, low noise and high power microwave performance and high current drive capability [1]-[2]. The main target of novel electronics technology is the fabrication of faster devices with the highest level of power and lowest level of noise figure [3]. Recently, heterostructure devices have provided superior performance than MESFETS. Preliminary researches have shown that noise properties of AlGa<sub>0.3</sub>N/GaN-HEMTs are comparable to those of AlGaAs/GaAs HEMTs [2]. AlGa<sub>0.3</sub>N/GaN-HEMT with 0.25 μm gate-length has demonstrated NF<sub>min</sub> of 0.77 dB at 5 GHz and NF<sub>min</sub> of 1.06 dB at 10 GHz [4]. AlGa<sub>0.3</sub>N/GaN-HEMT on SiC with a gate length of 0.15 μm showed NF<sub>min</sub> of 0.6 dB at 10 GHz [5]. An NF<sub>min</sub> of 0.98 dB at 18 GHz was achieved in AlGa<sub>0.3</sub>N/GaN-HEMT with a gate-length of 0.12 μm [1]. 0.2 μm AlGa<sub>0.3</sub>N/GaN-HEMT with a NF<sub>min</sub> of 1.5 dB at 26 GHz was reported [6]. AlGa<sub>0.3</sub>N/GaN-HEMT with 0.25 μm gate-length has demonstrated NF<sub>min</sub> of 0.75 dB at 10 GHz [3]. The purpose of this paper is to design of Al<sub>0.3</sub>Ga<sub>0.7</sub>N / GaN / Al<sub>0.06</sub>Ga<sub>0.94</sub>N / GaN HEMT transistor with extremely low noise figure while handling sufficient high power. The 2-D device simulator Silvaco ATLAS software is used for designing and simulation of device. The Silvaco software has high strong capability in semiconductor design and simulation analysis. Device exhibited NF<sub>min</sub> of 0.35 dB and maximum associated gain of 24.35 dB at 10 GHz. Also, device has demonstrated NF<sub>min</sub> of 0.51 dB and maximum associated gain of 22.3 dB at 18 GHz. To our knowledge, these are the best microwave noise characteristics of any GaN HEMTs ever reported with a 0.25 μm gate-length. The main task of this paper is explained completely in the following manner. The first part of this paper explains the device structure and layers detail. In the second part of this paper simulation results are explained. In this section, DC characteristics and microwave noise performance of device is explored. In the final part, the complete conclusion of this paper is explained.

### II. Device Structures

The cross section of the AlGa<sub>0.3</sub>N/GaN/AlGa<sub>0.06</sub>N/GaN HEMT with 0.25 μm-gate-length is shown in fig. 1. The layers are grown on a 3-μm SiC-4H substrate. The structure consists of a 2.5-μm-thick undoped GaN buffer layer, a 21-nm-thick AlGa<sub>0.06</sub>N bottom barrier layer with the Al composition 6%, a 14-nm-thick GaN channel layers and a 24-nm-thick Al<sub>0.3</sub>Ga<sub>0.7</sub>N top barrier layer. In order to optimize the channel electron density and comfort good ohmic contacts the AlGa<sub>0.06</sub>N schottky layer is selectively doped with Si [2]. Gate-source and gate-drain spacing is equal to 0.5 μm, 0.75 μm respectively. The metal work function for the gate schottky contact is (4.9eV). The material parameters of AlGa<sub>0.3</sub>N and GaN semiconductor are also included into the simulation that summarized in table I [7].

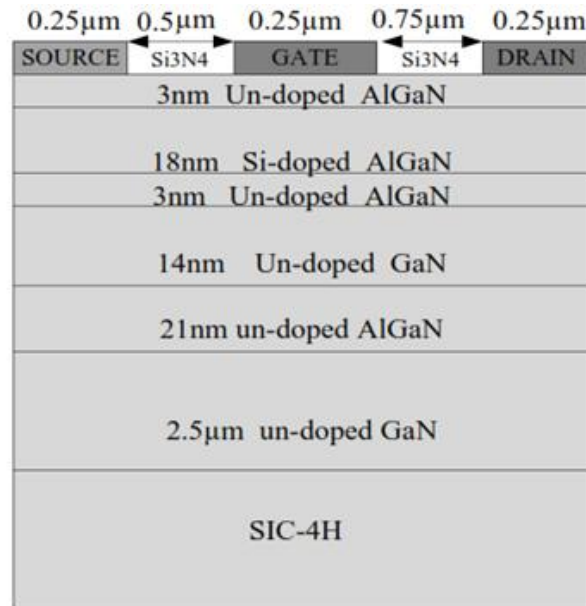


Fig. 1. Cross section of the AlGa<sub>N</sub>/Ga<sub>N</sub>/AlGa<sub>N</sub>/Ga<sub>N</sub> HEMT with 0.25 μm-gate-length

Table I. the material parameters of AlGa<sub>N</sub> and Ga<sub>N</sub> semiconductor

Material	Mobility ( $\mu$ )	Band gap (E <sub>g</sub> )	Affinity
Al <sub>0.3</sub> Ga <sub>0.7</sub> N	870	4.023 (ev)	2.97
Al <sub>0.06</sub> Ga <sub>0.94</sub> N	950	3.55	3.35
GaN	1300	3.42 (ev)	3.42

The polarization bar exists in the HEMT transistor based on Ga<sub>N</sub>, as a result the high drive current density is obtained. The polarization bar phenomena has been adapted in our simulation. In order to take the spontaneous and piezoelectric polarization into account in regions, POLARIZATION and CALC.STRAIN model is included. K.P model has been considered in our simulation for calculation effective masses and band gap energies in drift-diffusion device. To take account of recombination effects, we recommend the use of the Shockley-Read-Hall (SRH) model. High electric field velocity saturation is modelled through the field related mobility model (FLDMOB). Concentration mobility (CONMOB) model has been considered for estimation of the concentration dependent mobility effect. Auger model is used for recombination accounting for high level injection effects. Fig. 2 shows the conduction band profile in an AlGa<sub>N</sub>/Ga<sub>N</sub> HEMT at the equilibrium state. The two minimum point in the conduction band profile, placed at .029 μm and 0.059 μm, are clearly seen.

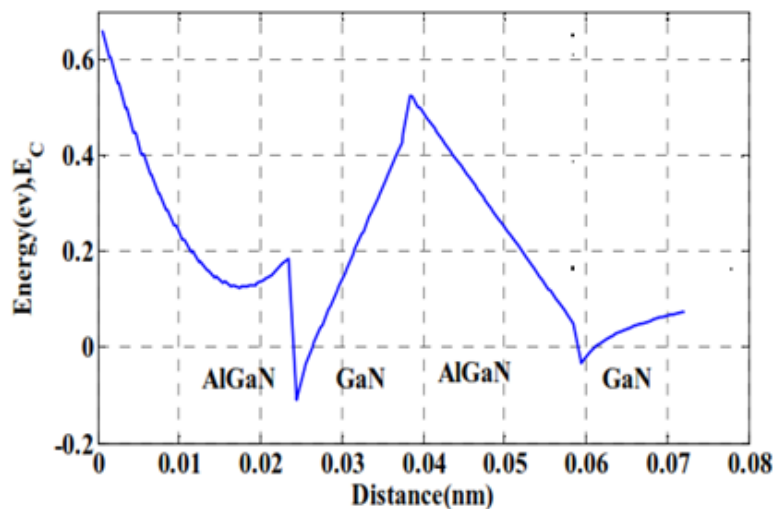


Fig. 2. Conduction band diagram E<sub>c</sub> of AlGa<sub>N</sub>/Ga<sub>N</sub>/AlGa<sub>N</sub>/Ga<sub>N</sub>-HEMT at the equilibrium state

### III. Dc Characteristic

Current-voltage (I-V) characteristics of a AlGaIn/GaN HEMT is simulated for the gate biases ( $V_{gs}$ ) from 0V to -6V in step of 0V, and for the drain biases from 0 to 15V, which is indicated in Fig. 3. Device depicted very high drain current drive capability. The maximum drain current was 1750ma/mm at a gate bias of 0V and a drain bias of a 13.5 V.

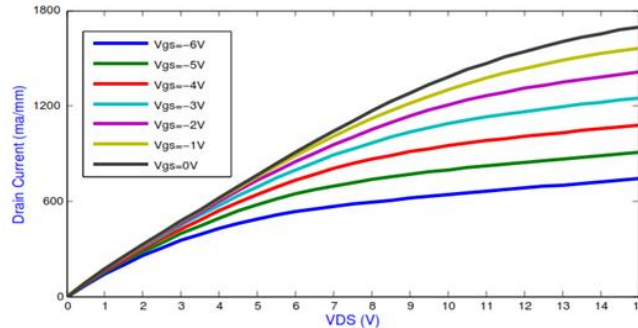


Fig. 3. I-V characteristics of AlGaIn/GaN/AlGaIn/GaN HEMT , the gate bias was swept from 0 V to -6 V

The dc transfer characteristics ( $I_D$ - $V_{GS}$ ) and transconductance of the 0.25  $\mu$ m AlGaIn/GaN HEMT are shown in Fig. 4 and Fig. 5. In both figures, the gate-source voltage ( $V_{gs}$ ) varies between -15 to 0 volt with a step 0.5 V. According to fig. 5, gate voltage increment results in an increased transconductance, because of the fact that the increased gate voltage causes the carrier concentration increasing in the channel. By more increasing the gate voltage, maximum transconductance is obtained. After this point, the transconductance will be decreased. In fact, a large gate voltage decreases the gate control on the channel, hence transconductance is reduced. By more increasing the gate voltage, vertical electric filed is increased in the channel, this filed causes the electrons mobility decrease in the channel, and hence, transconductance will be reduced. Drain voltage increment results in an increase in the gate control on the channel. Then transconductance is increased. Because of the increased drain voltage causes the electron concentration reduce in the parasitic channel in AlGaIn layer. By more increasing the drain voltage, lateral electric filed and electrons velocity will be increased in the channel and maximum transconductance is obtained. A peak extrinsic transconductance of 350 ms/mm was achieved at  $V_{gs} = -5V$  and  $V_{ds} = 12 V$ .

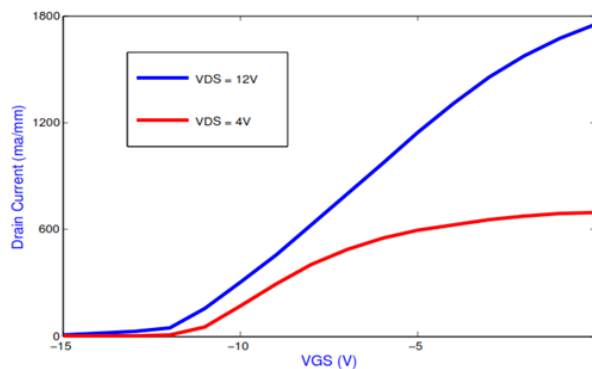


Fig. 4. ( $I_D$ - $V_{GS}$ ) for AlGaIn/GaN HEMT

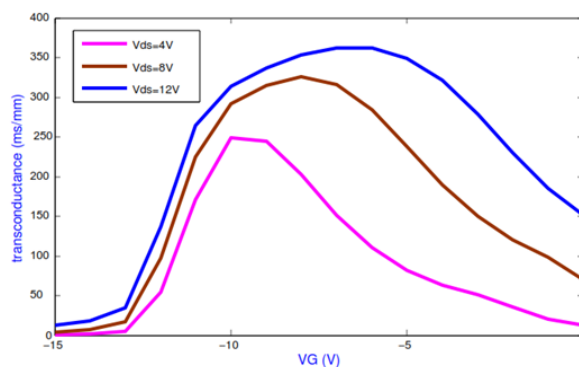


Fig. 5. (transconductance- $V_G$ ) at the different drain-source biases

#### IV. Microwave Noise Performance

Noise is very important factor in AlGa<sub>N</sub>/Ga<sub>N</sub> HEMT transistor. Impact ionization, tunneling current, change of carrier velocity, carrier generation and recombination provide the noise of the HEMT transistor. Silvaco has models for four types of microscopic noise source: diffusion noise, Impact ionization, generation-recombination noise, and flicker noise. Diffusion noise is caused by variations in the velocity of the carrier. Generation- recombination noise is caused by variations in the number of the carriers. There are two types of generation-recombination noise in silvaco: direct and trap assisted. Direct generation-recombination noise is when the electron travels directly from the conduction band to the valence band. Trap assisted is when the electron travels from a band to a trap level. Impact ionization is very important noise in AlGa<sub>N</sub>/Ga<sub>N</sub> HEMT transistor. For each electron crated in the conduction band, a corresponding hole is also created in the valence band. This is similar to direct generation-recombination noise without a recombination term. The different noise figure models introduced for heterostructure devices. Van der Ziel, Pucel, Fukui and Pospieszalski is the basis model of noise figure for HEMTs [2]. Fukui model is used in this paper for showing microwave noise performance of the proposed structure. The noise parameters of this model are [2]:

$$NF_{\min} = 1 + k_1 \times f \times C_{gs} \times \sqrt{\frac{R_s + RG}{gm}} \quad (1)$$

$$R_{opt} = K_3 \times \left[ \frac{1}{4gm} + RS + RG \right] \quad (2)$$

$$X_{opt} = \frac{K_4}{f \times cgs} \quad (3)$$

The variables K1 to K4, are the fitting parameters, and will change with the device technology and bias. Fig. 6 and fig. 7 shows a minimum noise figure (NFmin) and maximum associated power gain (Gma) versus frequency for the 0.25 um AlGa<sub>N</sub>/Ga<sub>N</sub> HEMT. The device was biased at V<sub>ds</sub> = 10 V and V<sub>gs</sub> = -3 V. Device exhibited a NFmin of 0.35 dB and a (Gma) of 24.35 dB at 10 GHz. In the frequency limit of 3 GHz-20 GHz Gma ranges from 29.12 dB to 21.82 dB and NFmin is in the range of 0.14 dB to 0.54 dB. Aluminum mole fraction increment plays major role in noise decrement in the proposed structure. Aluminum mole fraction increment in the AlGa<sub>N</sub> layer, increases the polarized carrier density and hence the electric filed is increased. Aluminum mole fraction increment in the AlGa<sub>N</sub> layer results in the 2DEG depth increment. As a result, electron density in the 2DEG region is increased. Therefore, device transconductance (gm) increases and due to equation (1), the device noise is reduced.

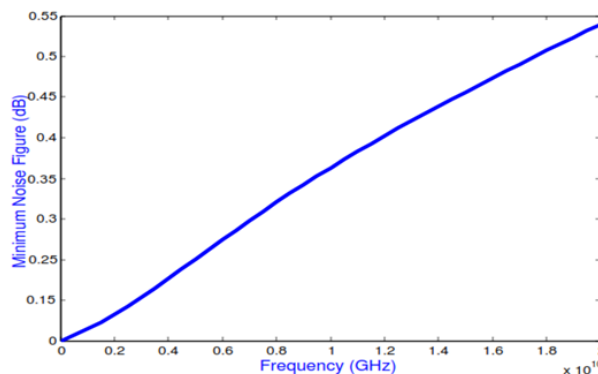


Fig. 6. (NFmin-F), at the V<sub>ds</sub> = 10 V and V<sub>gs</sub> = -3 V

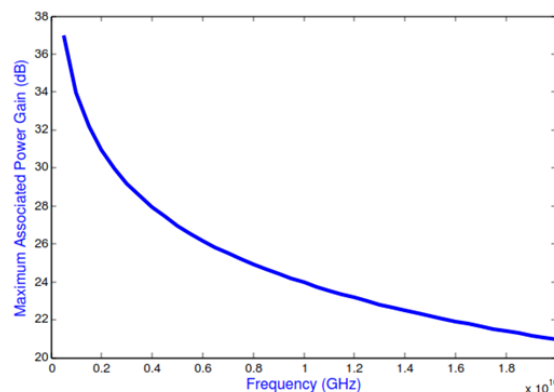
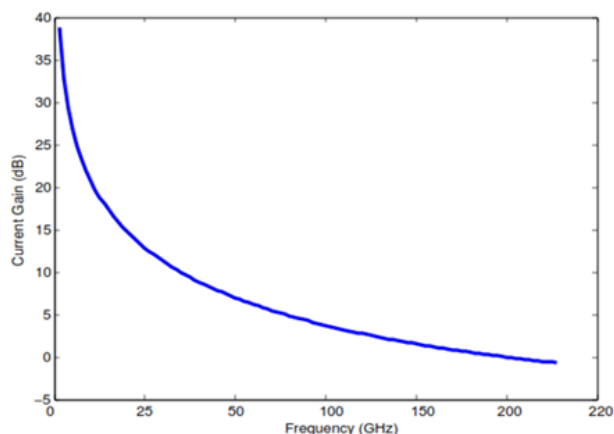


Fig. 7. (Gma-F), at the V<sub>ds</sub> = 10 V and V<sub>gs</sub> = -3 V

Fig. 10 indicate the unity current gain cut-off frequencies ( $f_t$ ) of device against frequency at  $V_{ds}=12v$  and  $V_{gs} = -5.5 V$ . The ( $f_t$ ) of device is equal to 200 GHz.



**Fig. 10.** Current gain cut-off frequencies ( $f_t$ ) as a function of frequency

## V. Conclusion

In this paper, AlGaIn/GaN/AlGaIn/GaN HEMT on SiC substrate with a gate length of 0.25  $\mu m$  has been designed and simulated. The device exhibited a high current drive capability of 1750 mA/mm. The peak extrinsic transconductance of device is equal to 350 mS/mm. The microwave noise performance of proposed structure was explored. The device exhibited excellent noise performance. An NFmin of 0.35 dB and a Gma of 24.35 dB have been obtained at 10 GHz and  $V_{ds}=10 V$  as follow as  $V_{gs}=-3 V$ . All these superb DC and microwave noise characteristics indicate the potential of AlGaIn/GaN-HEMT transistor for design of low noise amplifier in microwave frequency range. The simulation results have good assent with desired demand.

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